



coreform

Isogeometric analysis using the
*IGA_INCLUDE_BEZIER keyword
in LS-DYNA

Matthew Sederberg, Coreform CEO

Agenda

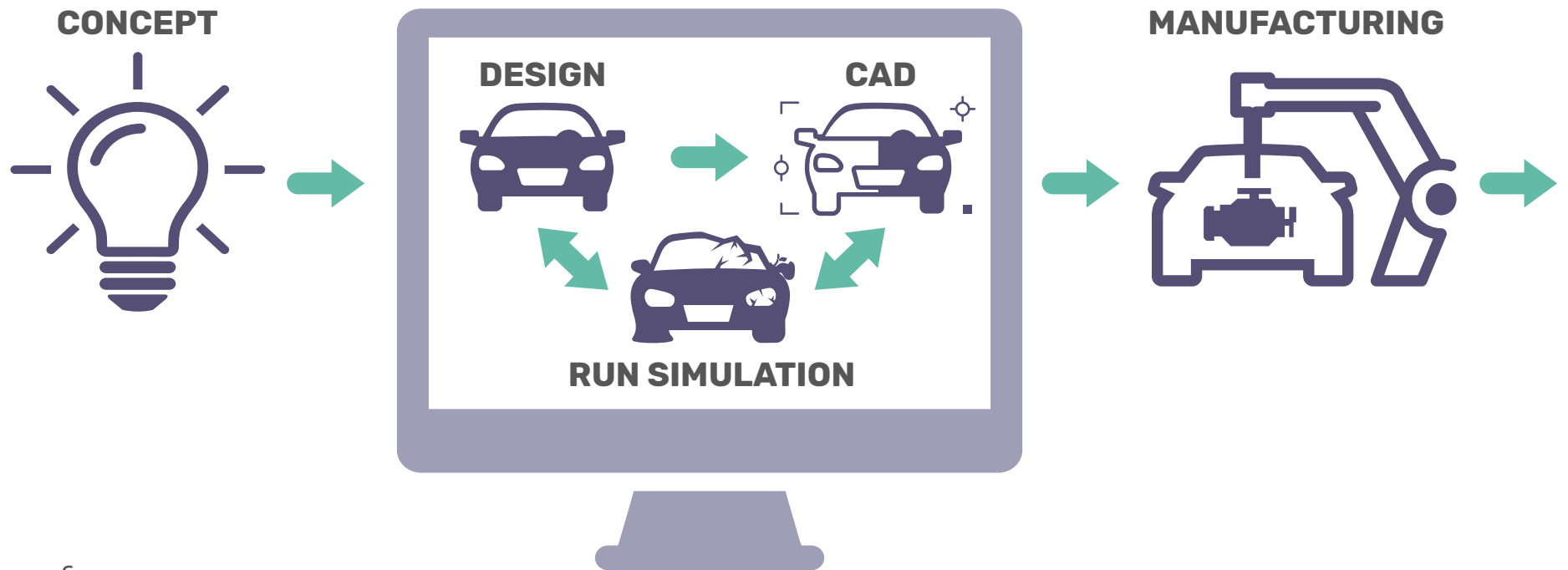
- Value of *IGA_INCLUDE_BEZIER
 - Isogeometric analysis
 - Unstructured splines
 - Larger explicit time steps
- How to use *IGA_INCLUDE_BEZIER
- Future possibilities

Spline-based simulation papers since 2005

USA - 502	China - 332	Germany - 315	Italy - 265	S Korea - 183	Vietnam - 118
Austria - 105	Iran - 101	Spain - 94	Japan - 87	England - 83	France - 78
Netherlands - 68	Australia - 67	Belgium - 64	Saudi Arabia - 53	India - 52	Norway - 45
Wales - 41	Switzerland - 36	Scotland - 41	Poland - 28	Luxembourg - 27	Singapore - 27
Canada - 26					



Vision of isogeometric analysis (IGA): A single source of truth for design and analysis



Using highly accurate spline-based FEA

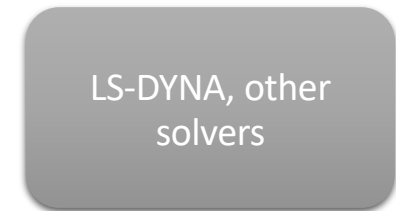
- FEA mesh data



Nastran

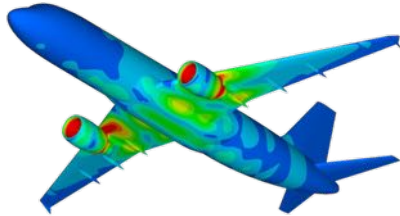


- Next-gen CAD data

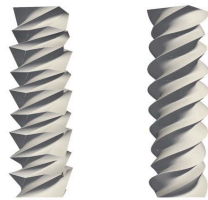


Promise of smooth spline-based FEA

Better simulation through better geometry



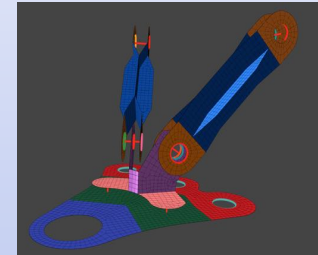
Better
accuracy in
less time



Increased
robustness

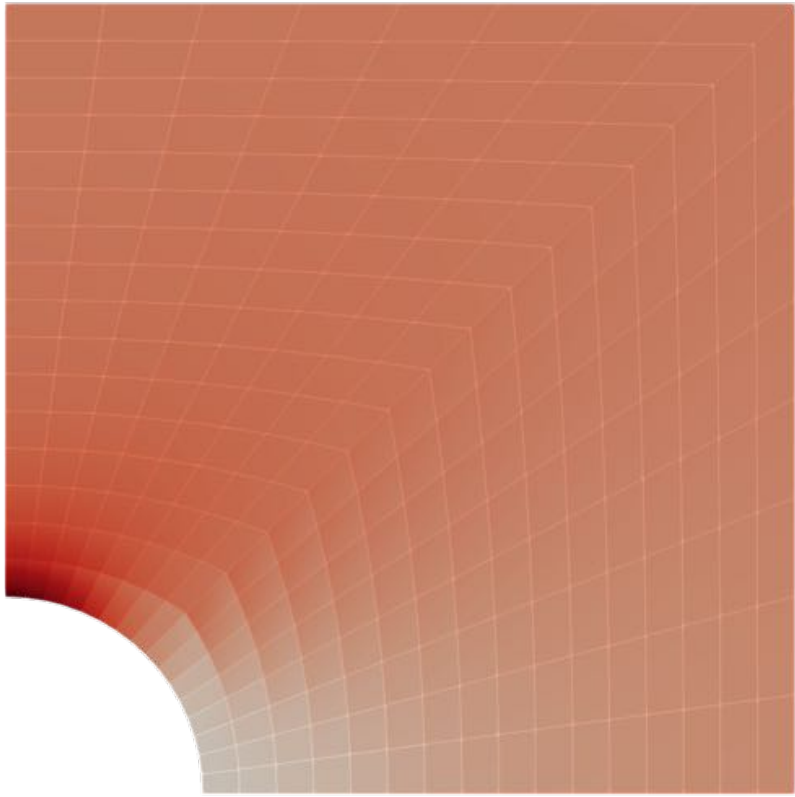


Lower
simulation
costs

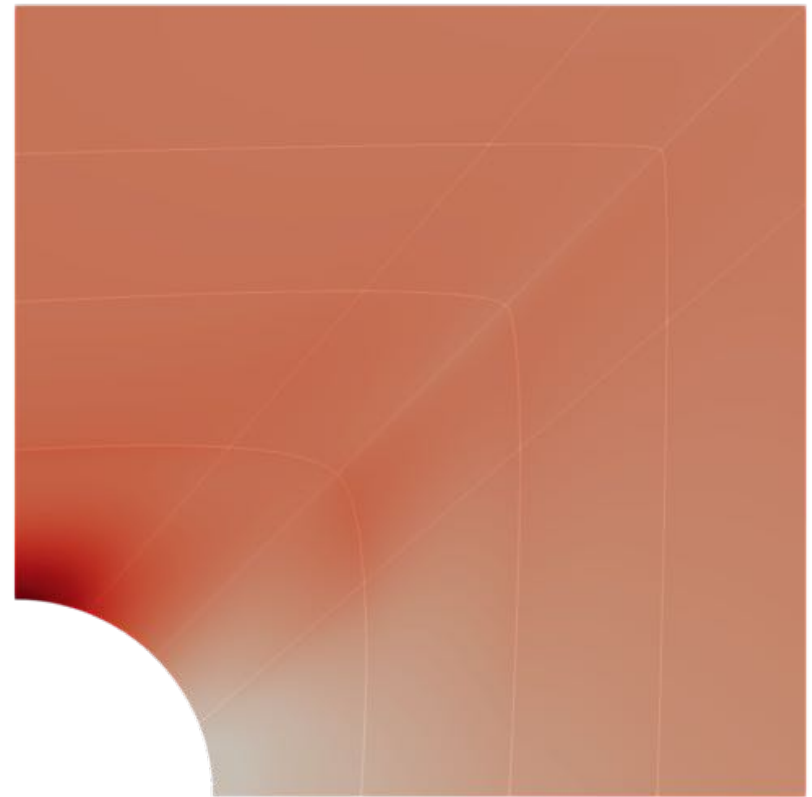


Minimal
change to your
workflow

Better stress accuracy: 16x fewer elements for ~1% error



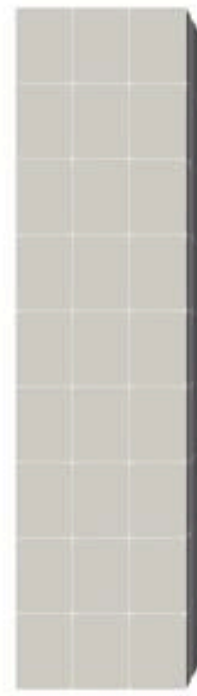
FEA: 256 elements



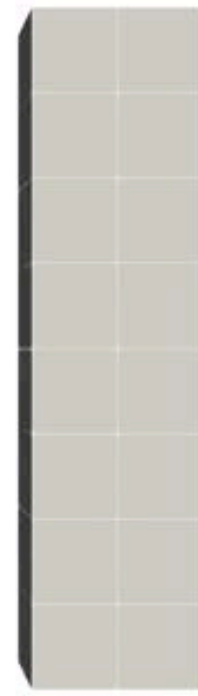
Splines: 16 elements

Splines are more robust for large deformations

	FEA	Spline
Degree	1	2
# of nodes	160	160
Timesteps completed	144	209



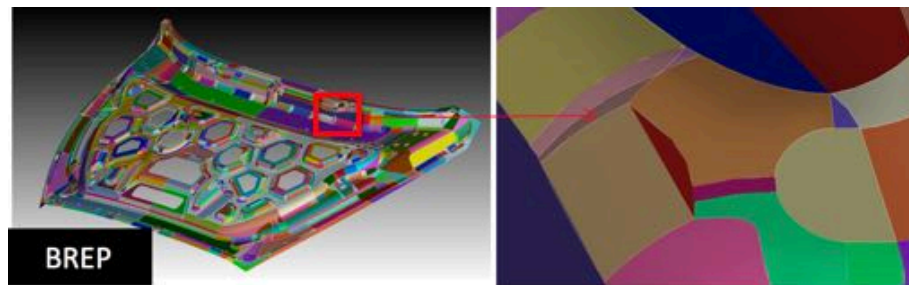
FEA



Splines

U-splines: next-gen CAE/CAD technology

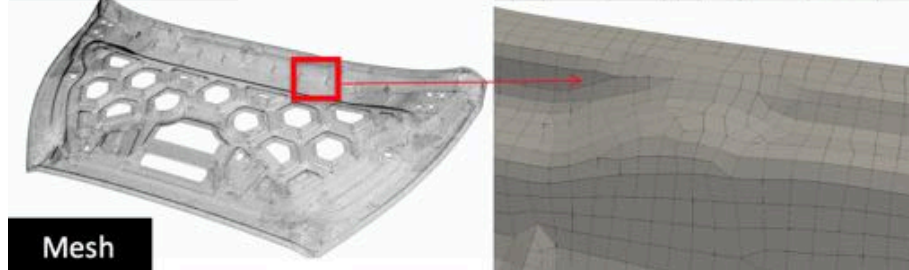
Traditional
engineering
design



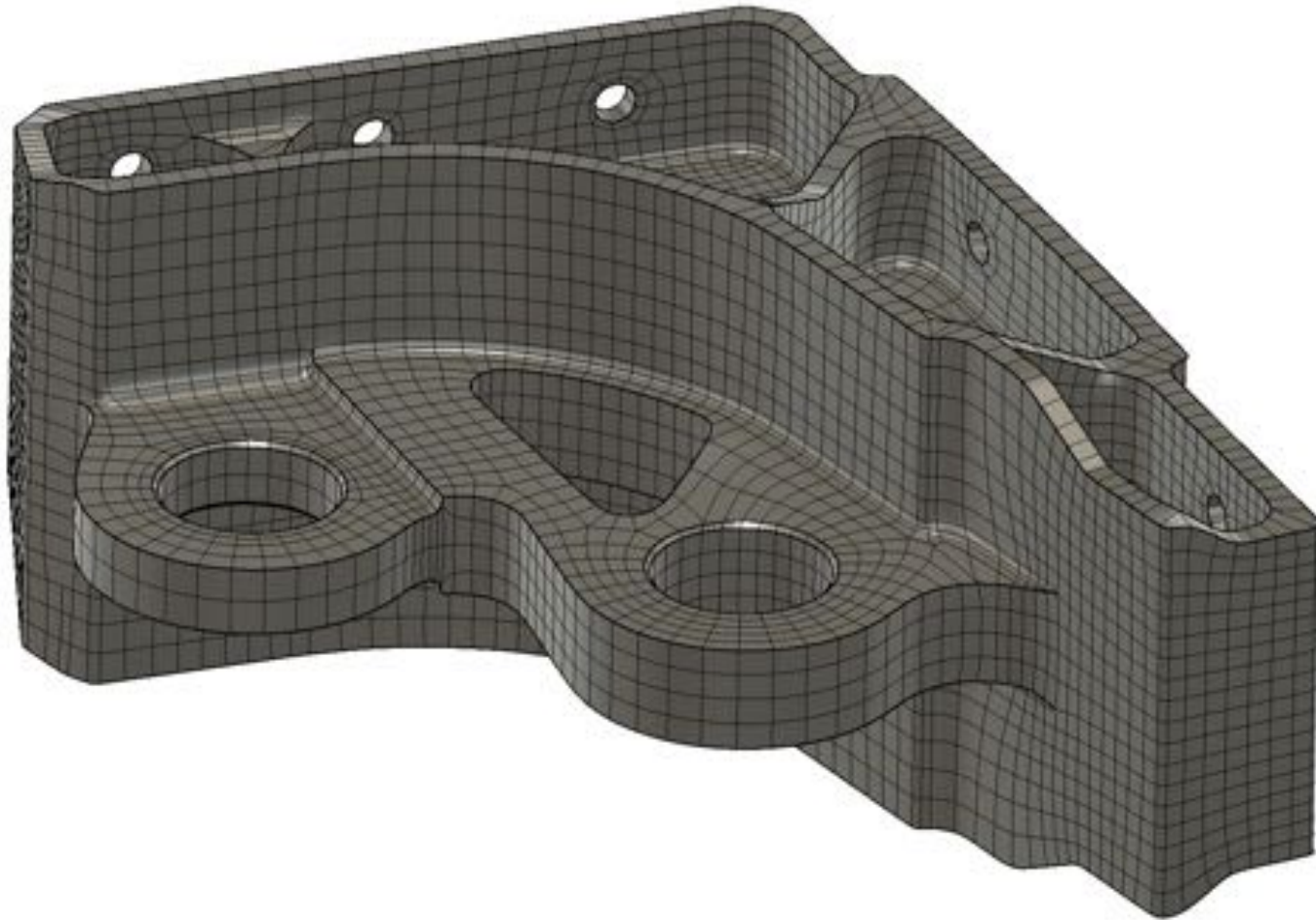
Next-gen
design and
analysis



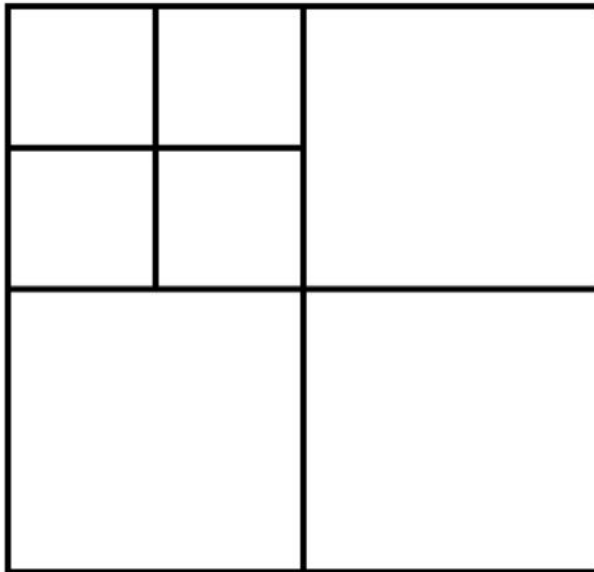
Traditional
engineering
analysis



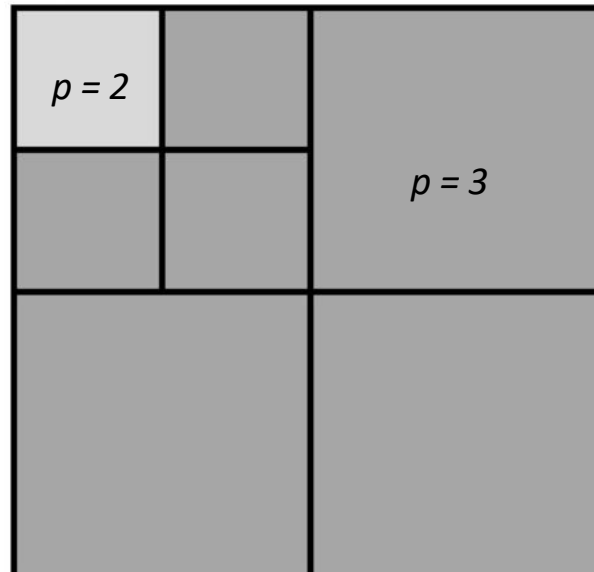
Analysis-suitable geometry



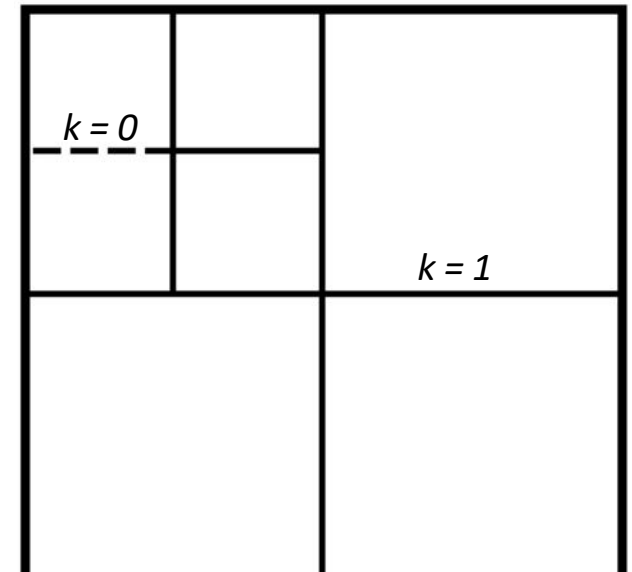
Non-uniform topology



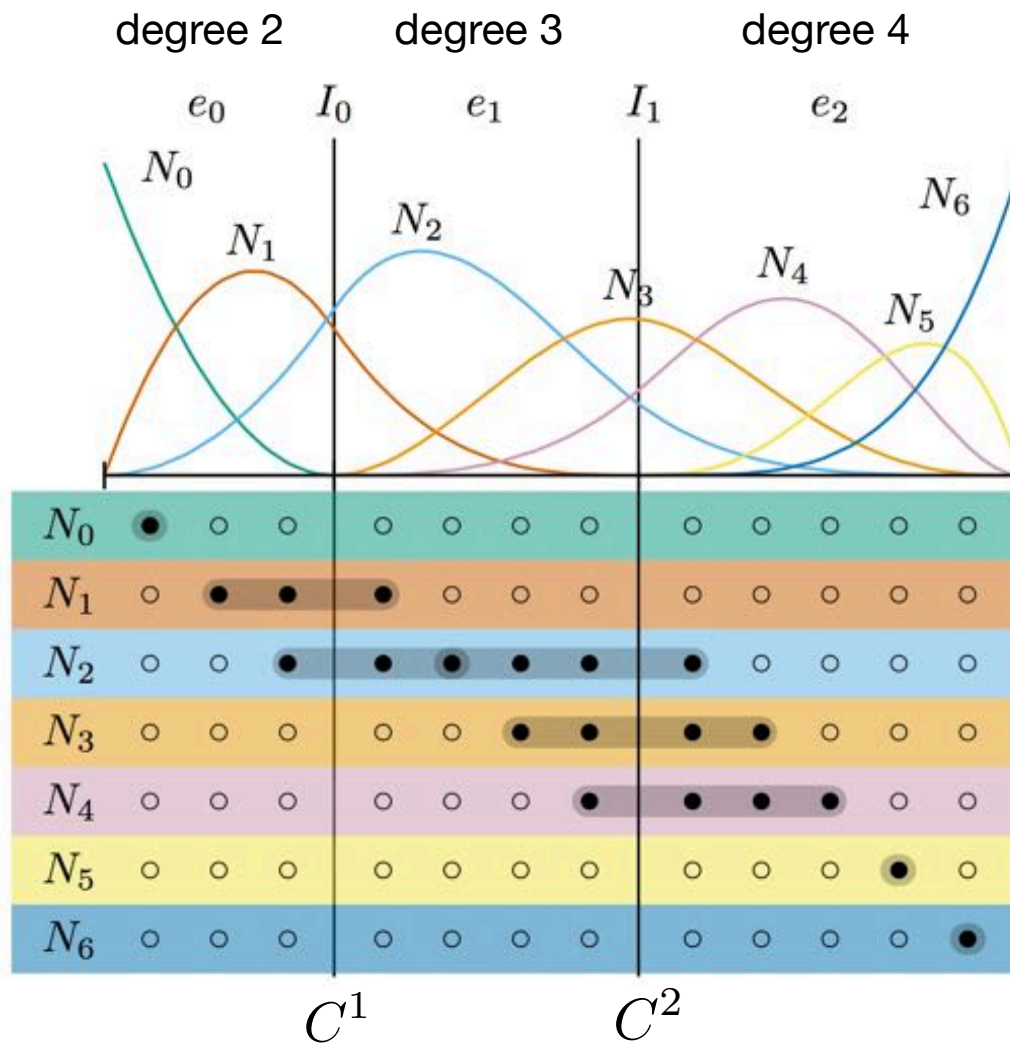
Non-uniform degree



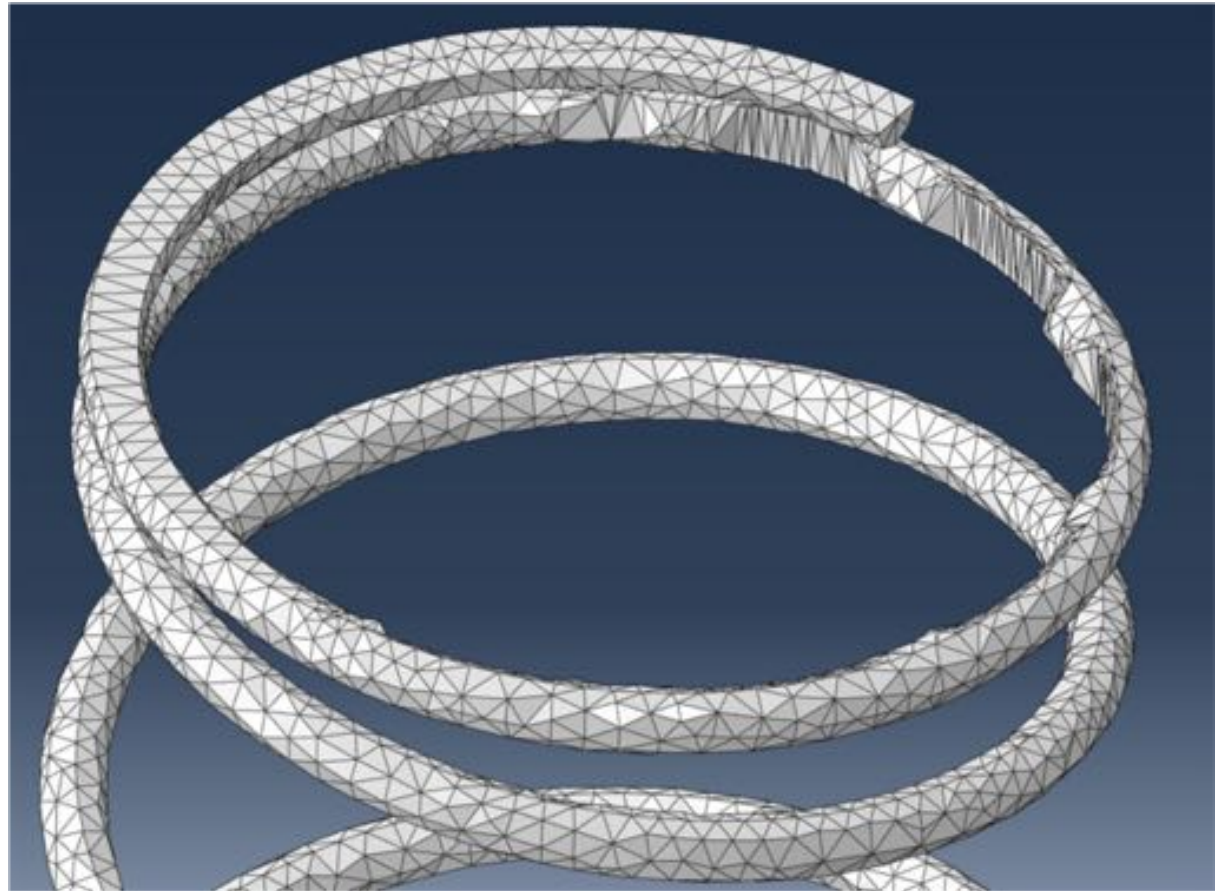
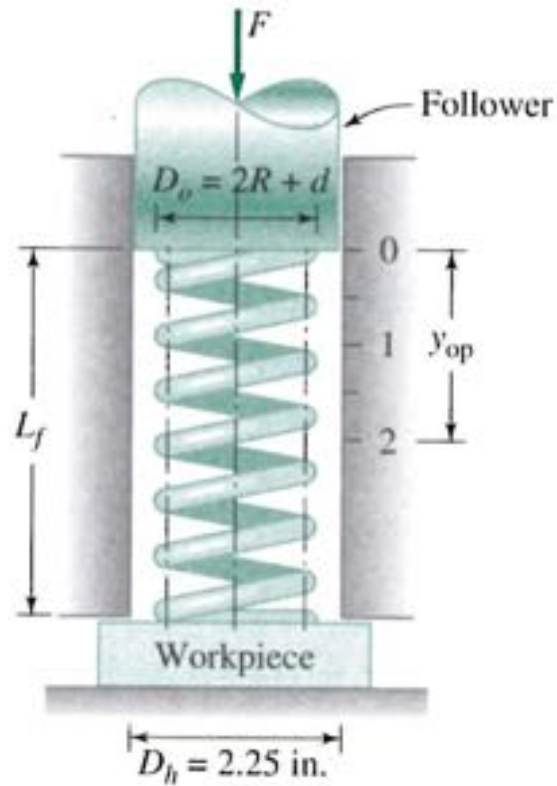
Non-uniform smoothness



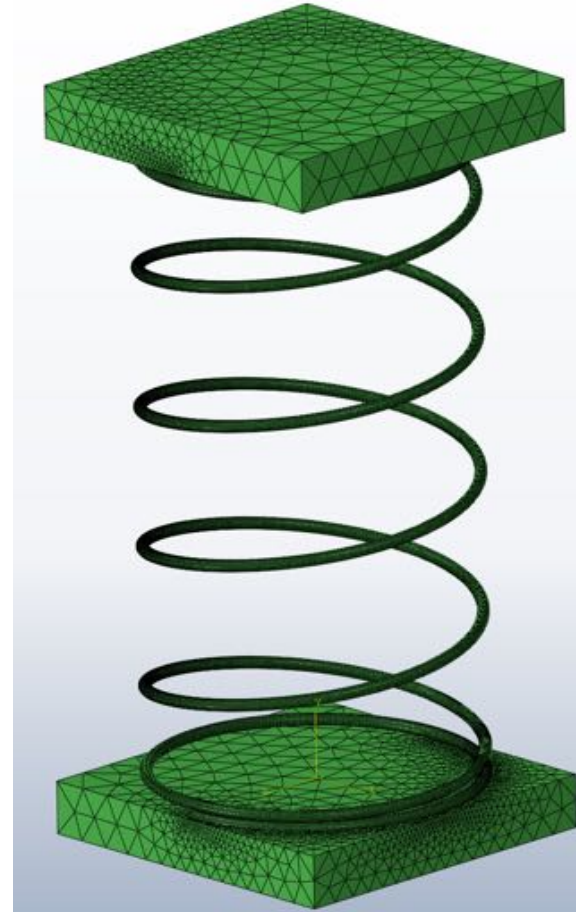
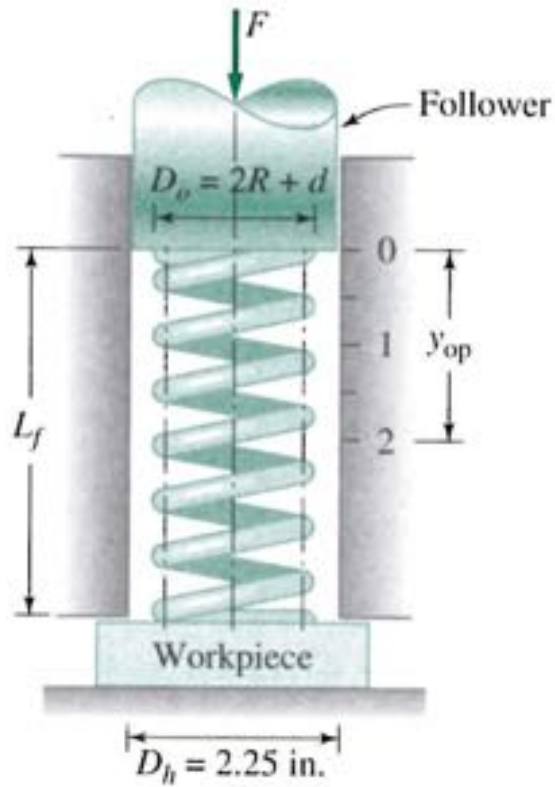
- Partition of unity
- Compactly supported
- Positive
- Linearly independent



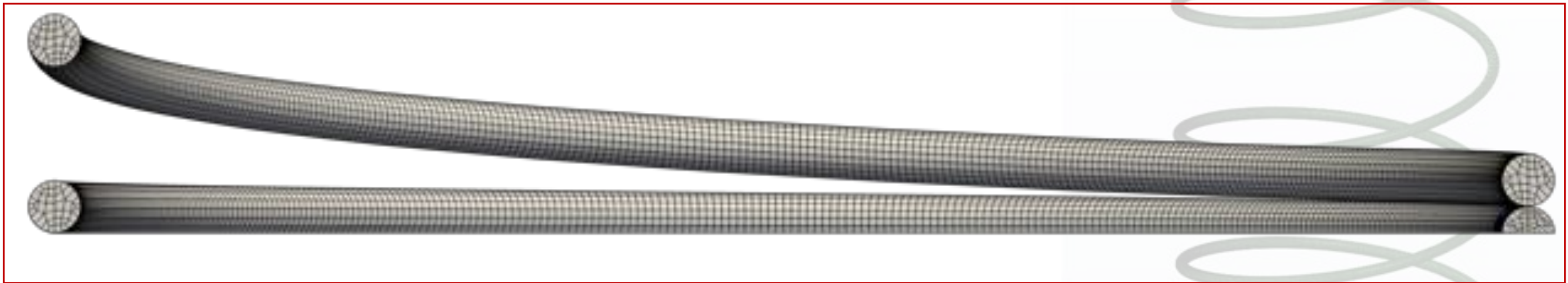
Better accuracy with less time and effort



Better accuracy with less time and effort



Better accuracy with less time and effort



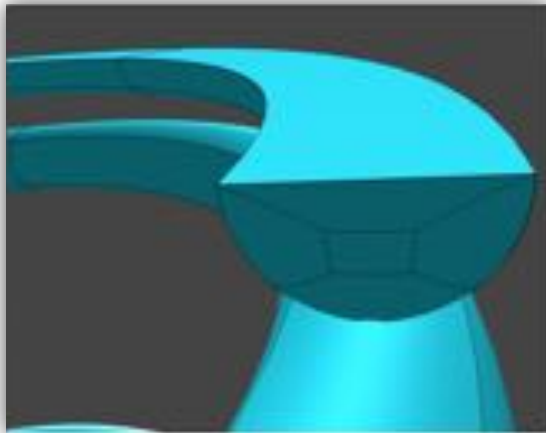
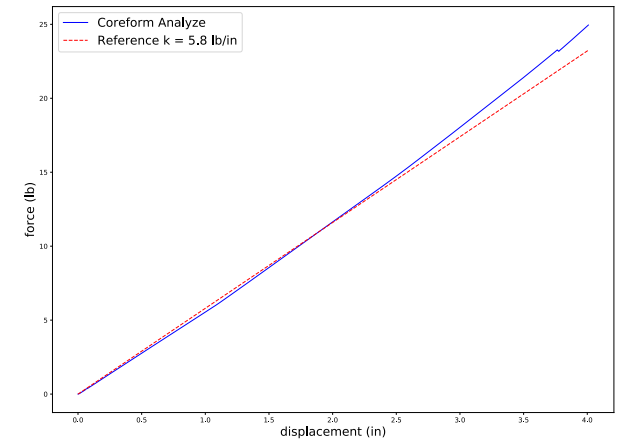
225,000 small elements required to capture curvature with FEA!



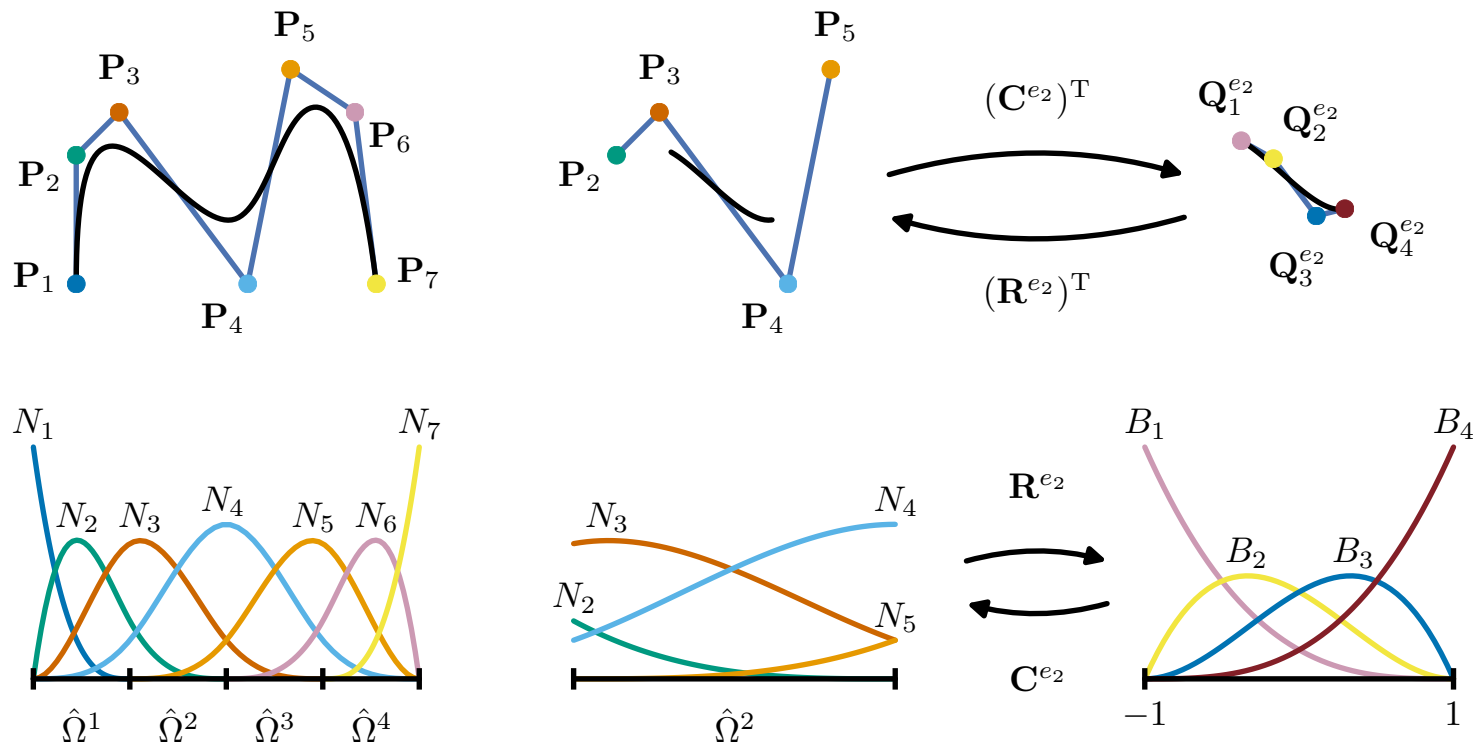
Project shared by permission, funded by Honeywell

Better accuracy: 50x faster, 500x fewer elements

	FEA	U-Splines
Elements	225,000	500
Total compute hours	384	8



Bézier extraction: Equivalence between Bézier and B-spline representations



*IGA_INCLUDE_BEZIER

Purpose: import complex spline data into LS-DYNA

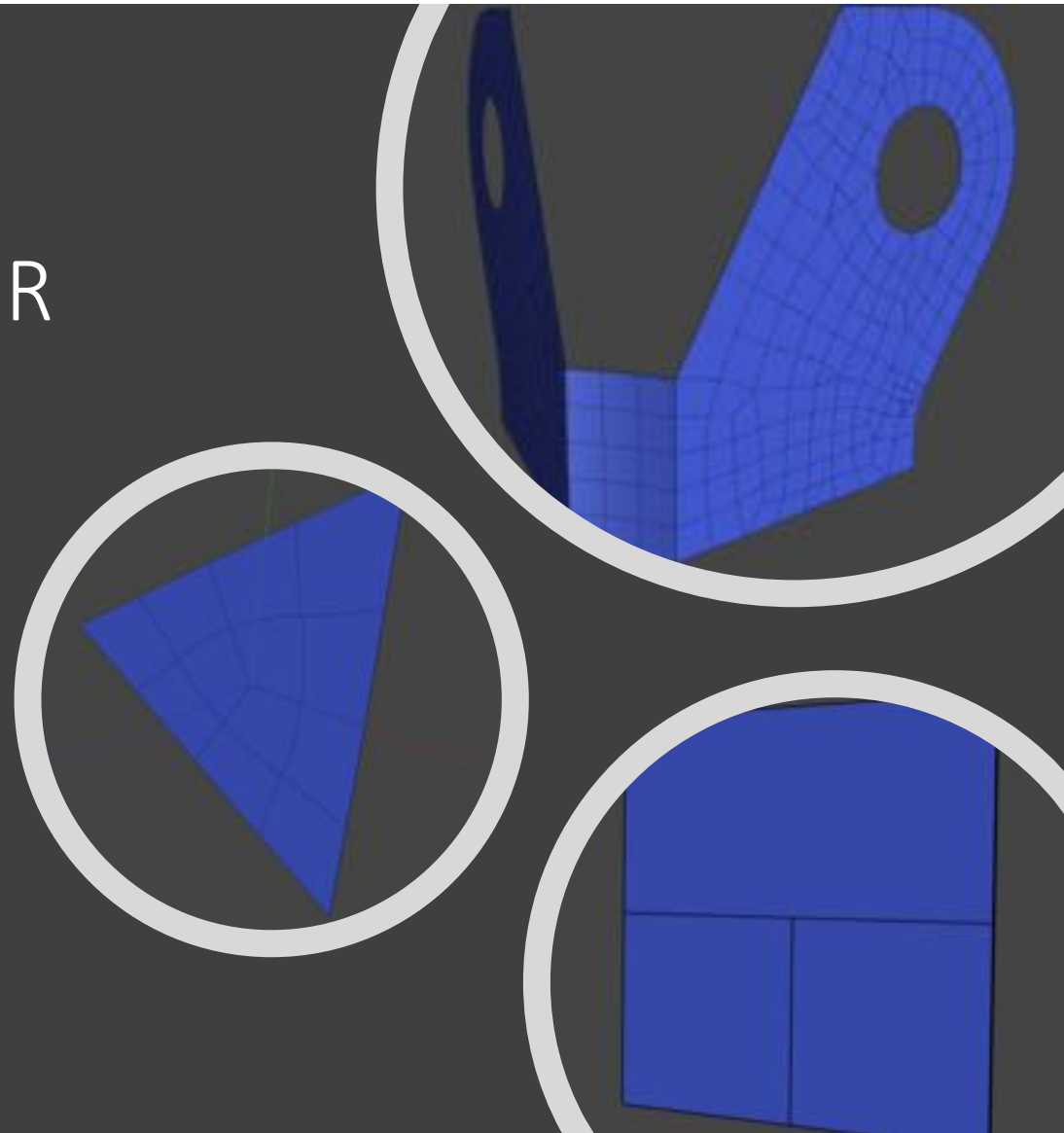
- Improvement over old Bezier extraction keyword
- Allows for simplex and prism elements
- More efficient data storage

Current status

- Still under active development
- Beta version: scheduled for summer of 2019
- Public availability: scheduled for Rev 12 of LS-DYNA Keyword Manual

*IGA_INCLUDE_BEZIER format

- Patch data
- Geometry
- Elements descriptions
- Coefficient vectors



*IGA_INCLUDE_BEZIER features:

1. Increased explicit time step size
2. Import of solid spline models
3. Import of T-spline CAD models
4. Smoothing of unstructured FEA meshes via U-splines
5. Future possibility of IGA assembly models in LS-DYNA

1. Increase explicit time step size



The central difference method

Evolution Through Time

$$\mathbf{M}\mathbf{a}_{n+1} = \mathbf{R}_{n+1}(\mathbf{d}_{n+1})$$

$$\mathbf{d}_{n+1} = \mathbf{d}_n + \Delta t \mathbf{v}_n + \frac{\Delta t^2}{2} \mathbf{a}_n$$

$$\mathbf{v}_{n+1} = \mathbf{v}_n + \frac{\Delta t}{2} (\mathbf{a}_n + \mathbf{a}_{n+1})$$

Stability Condition

$$\Delta t \leq \frac{2}{\omega_{max}^h}$$

n = Time step number

Δt = Time step size

\mathbf{d} = Displacement

\mathbf{v} = Velocity

\mathbf{a} = Acceleration

\mathbf{M} = Mass matrix

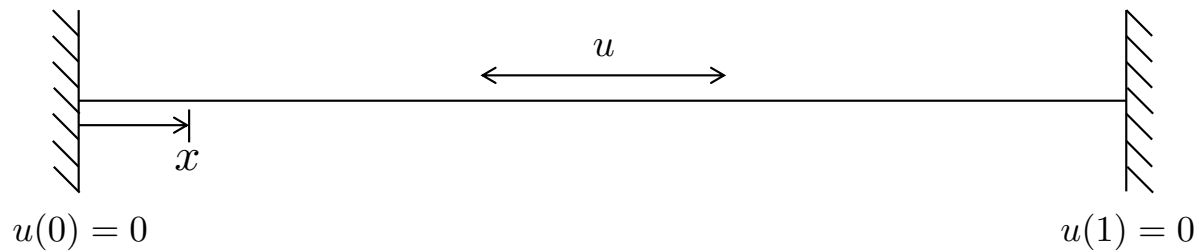
\mathbf{R} = Residual, note that \mathbf{R}_{n+1}
is independent of \mathbf{a}_{n+1}

ω_{max}^h = Maximum discrete frequency

1D vibrating rod

$$L = E = \rho = 1$$

$$\frac{\partial^2 u}{\partial x^2} + \omega^2 u = 0$$



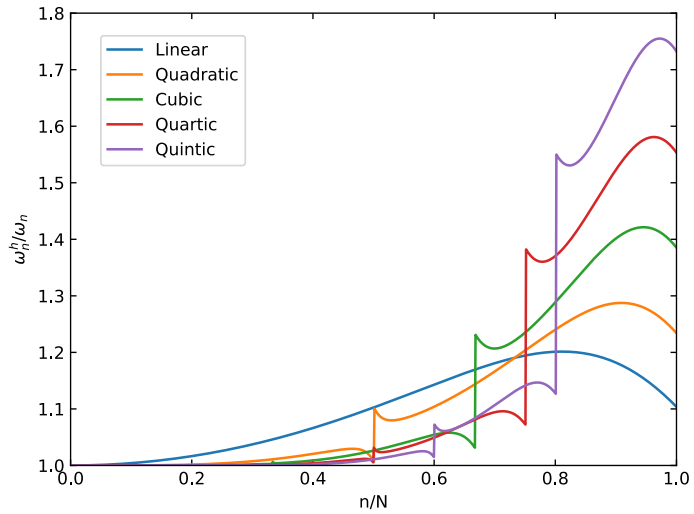
Exact modes:

$$u_n = \sin(n\pi x)$$

$$\omega_n = n\pi$$

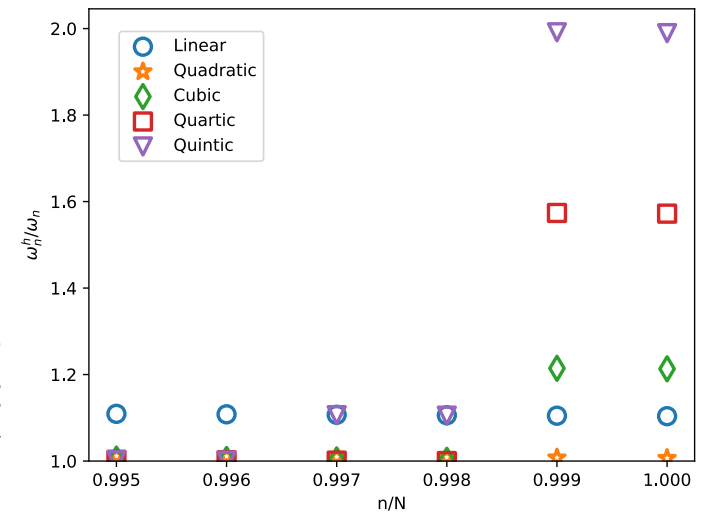
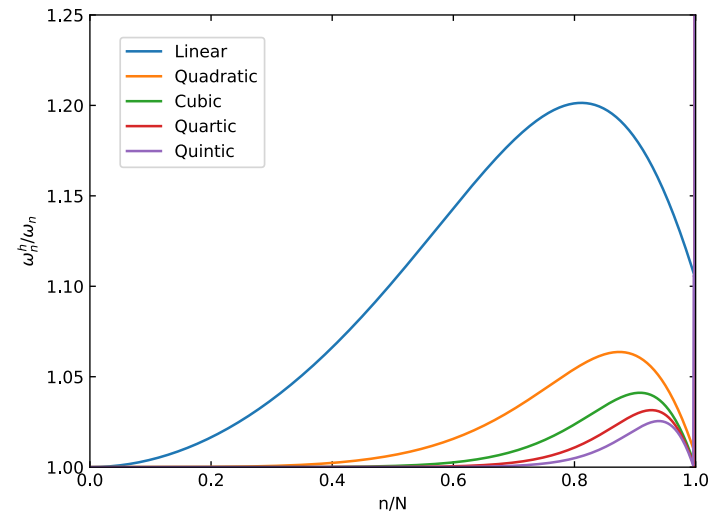
for $n = 1, 2, 3, 4, \dots$

Lagrange



n = Mode number
 N = Number of DOFs
 ω_n = Exact n th frequency
 ω_n^h = Discrete n th frequency

NURBS



Raising continuity helps most of the spectrum, but not the highest frequency



The challenge of increasing degree

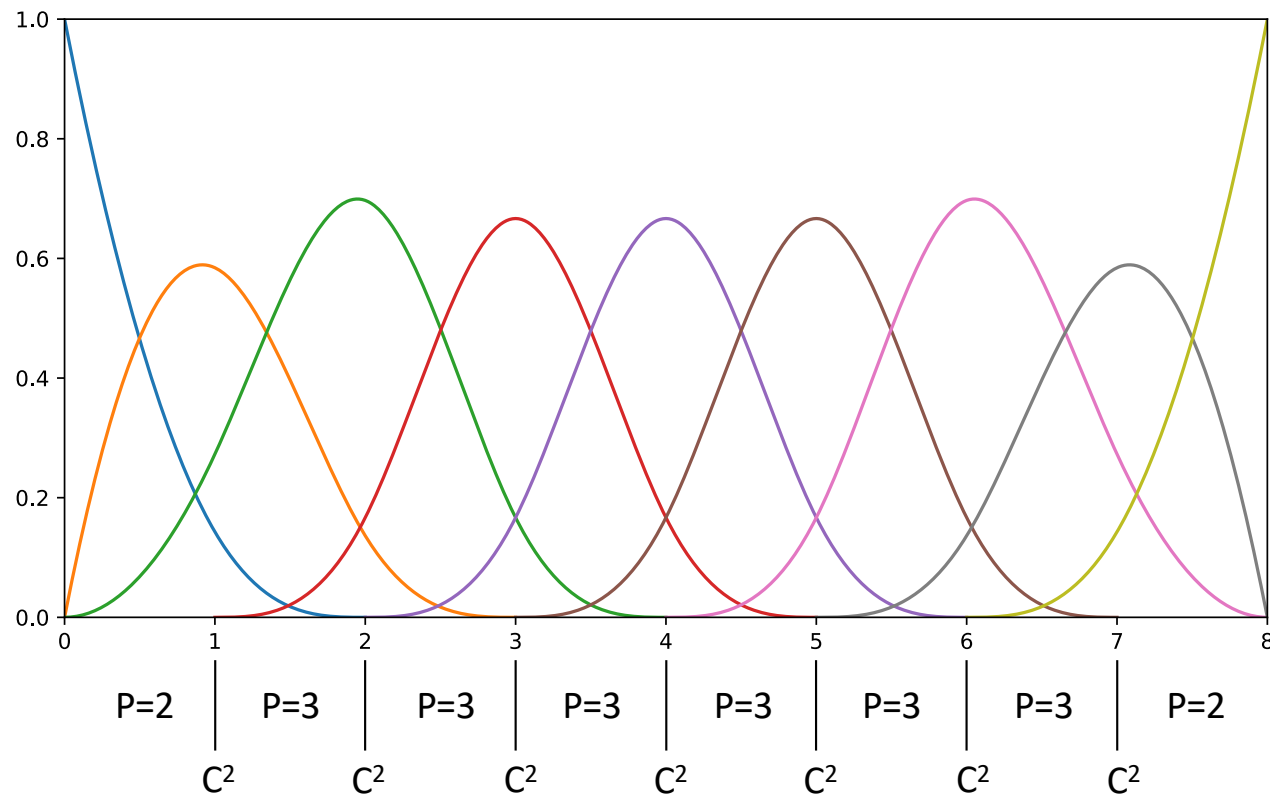
Increase degree



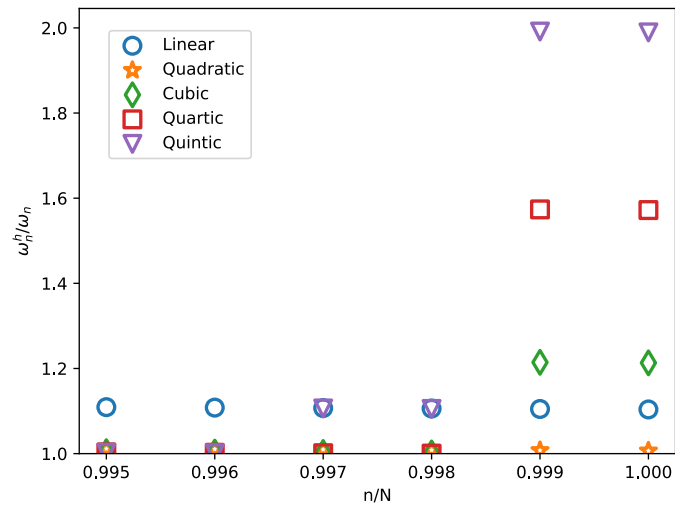
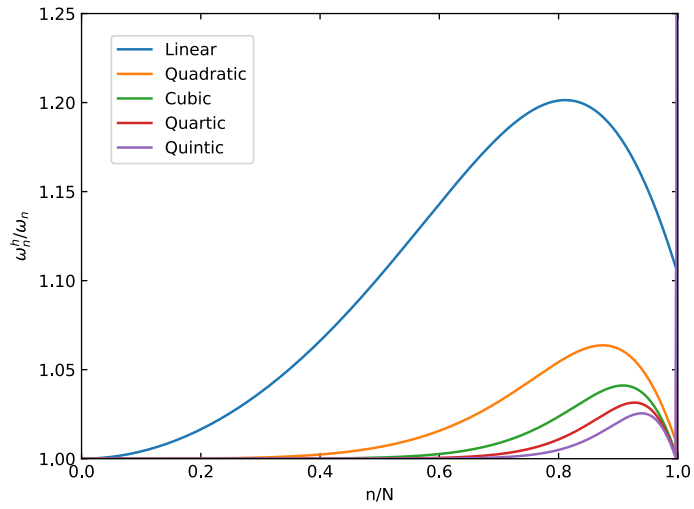
Decrease time step

- Lagrange
- **Multi-patch NURBS**
- T-splines
- etc.

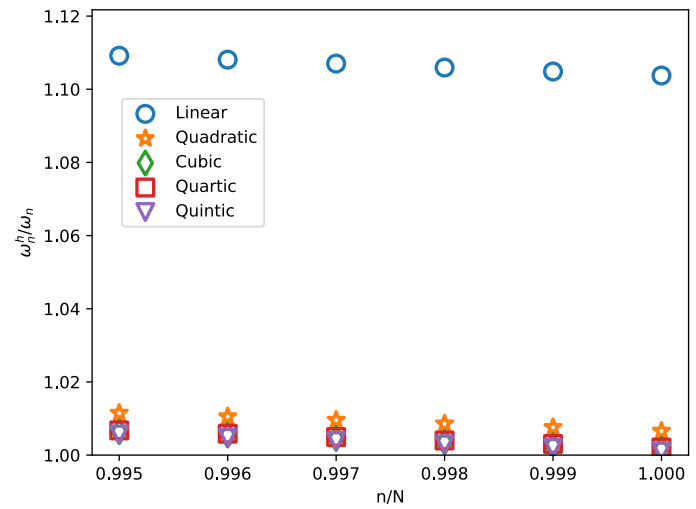
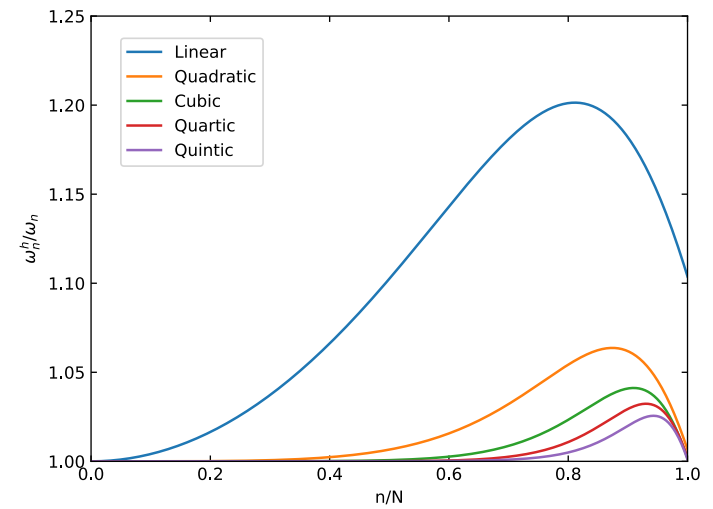
U-splines can uniquely increase the time step



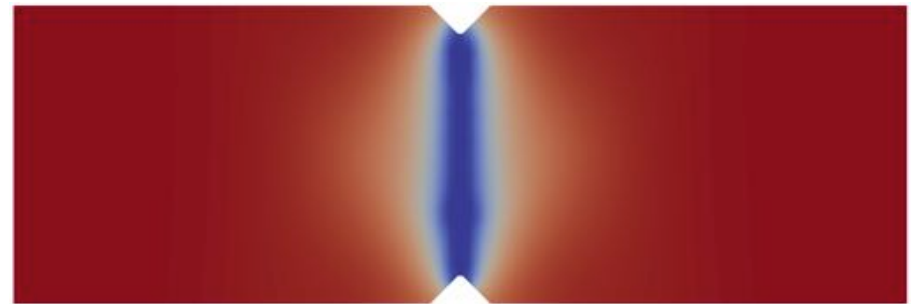
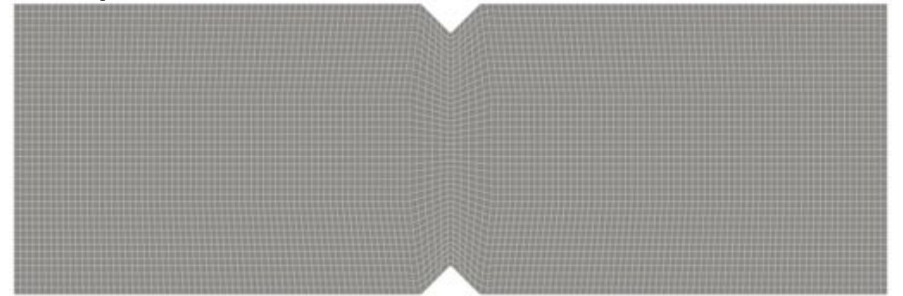
NURBS



U-splines



Time step example: v-notch problem

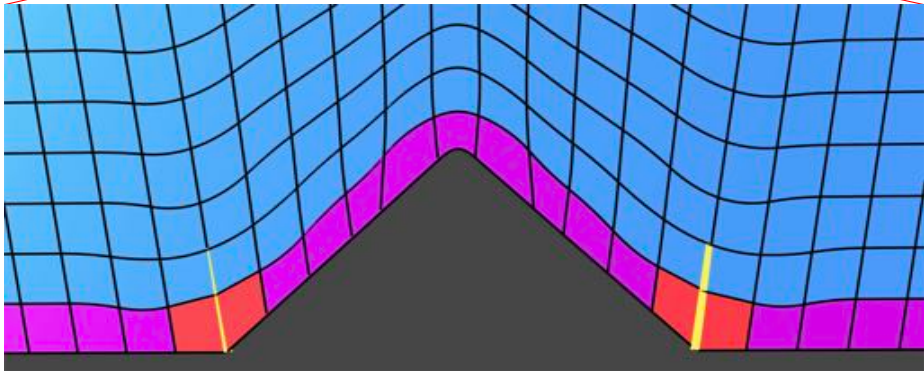
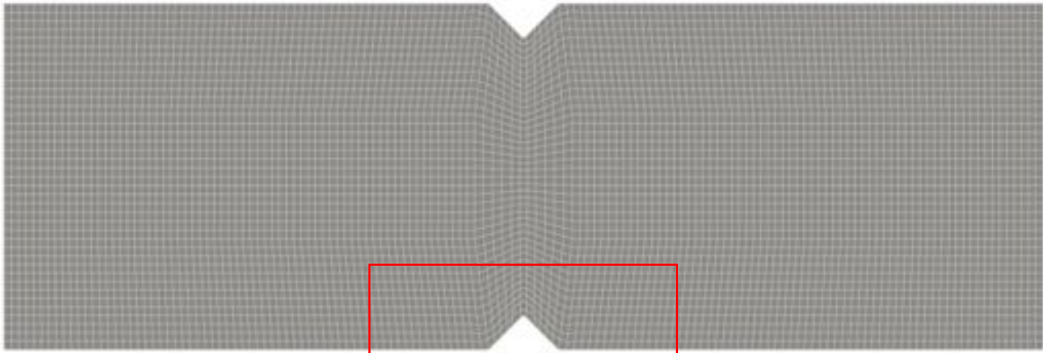


Crack formation



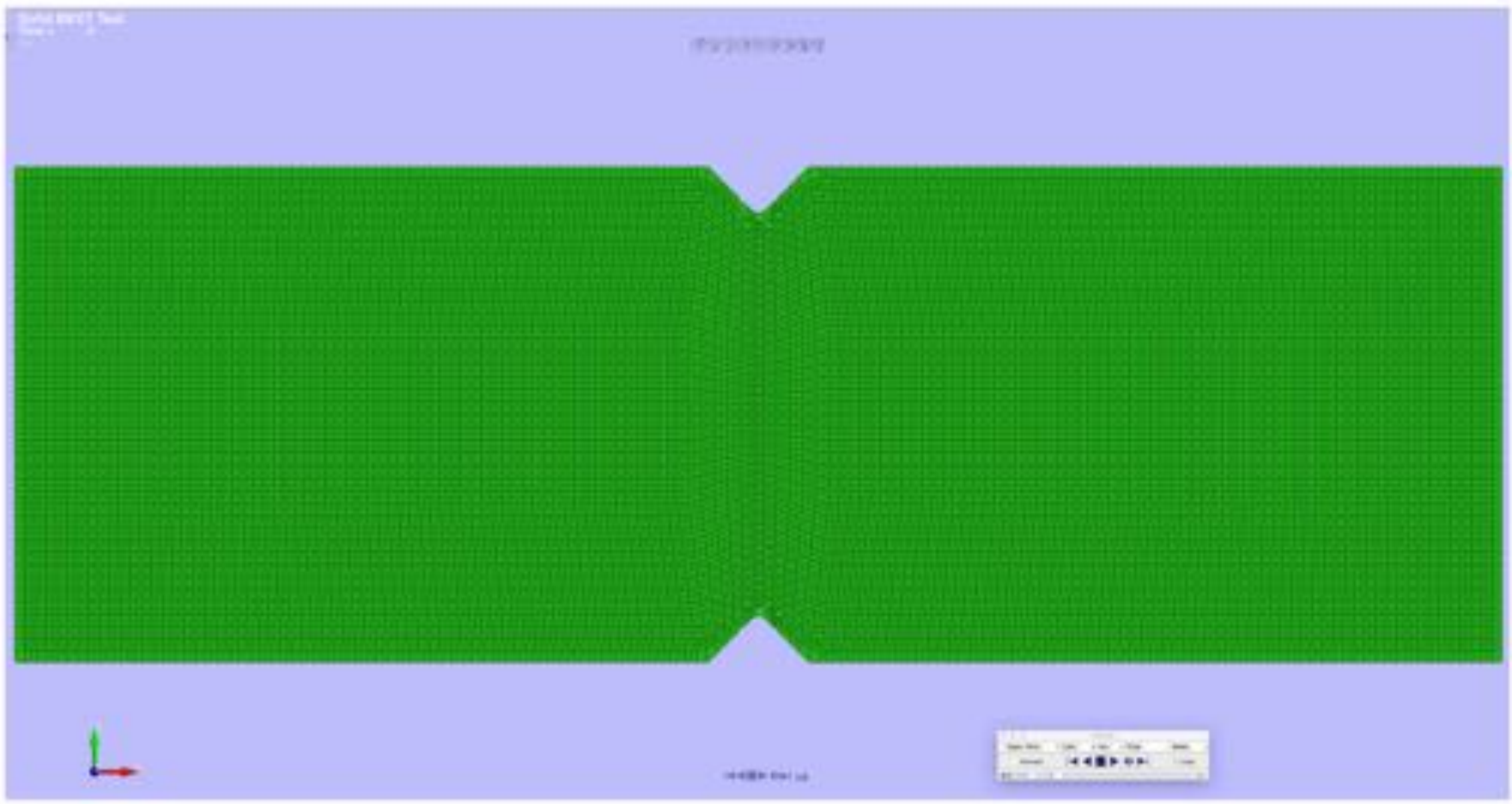
Crack after fracture

Optimized U-Spline basis



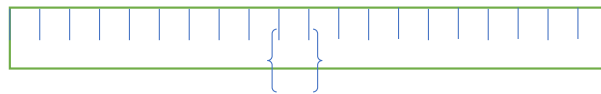
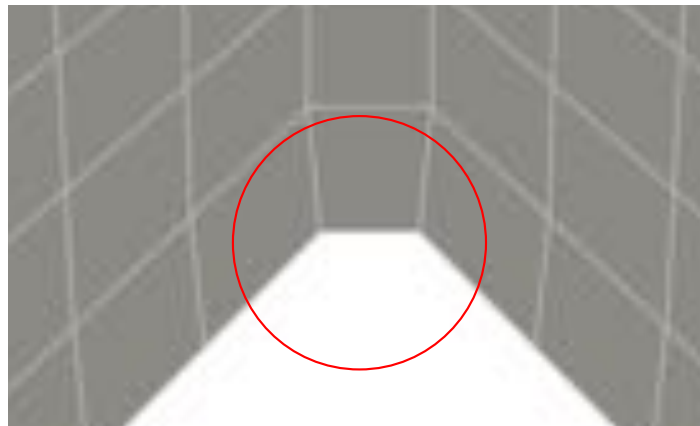
	Bi-Quadratic
	Bi-Linear
	Mixed Quadratic-Linear
	C0 Continuity
	C1 Continuity

Optimized U-Spline in LS-DYNA via *IGA_INCLUDE_BEZIER



Lower simulation costs

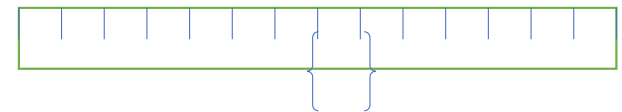
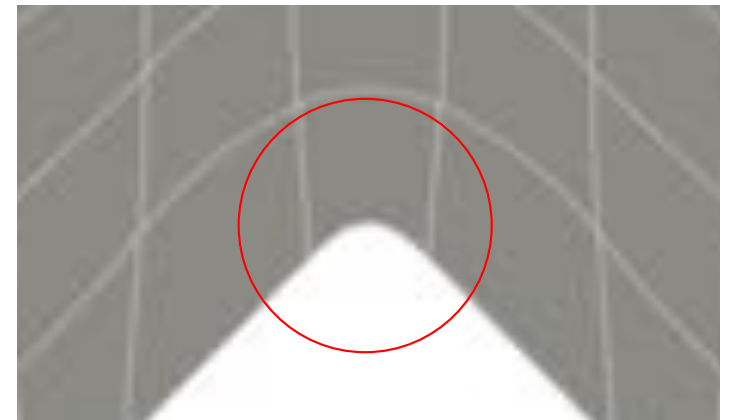
FEA



Time step: 1.35×10^{-7}

Smooth fillet captured!

U-splines



Time step: 2.18×10^{-7}

60% larger time step!

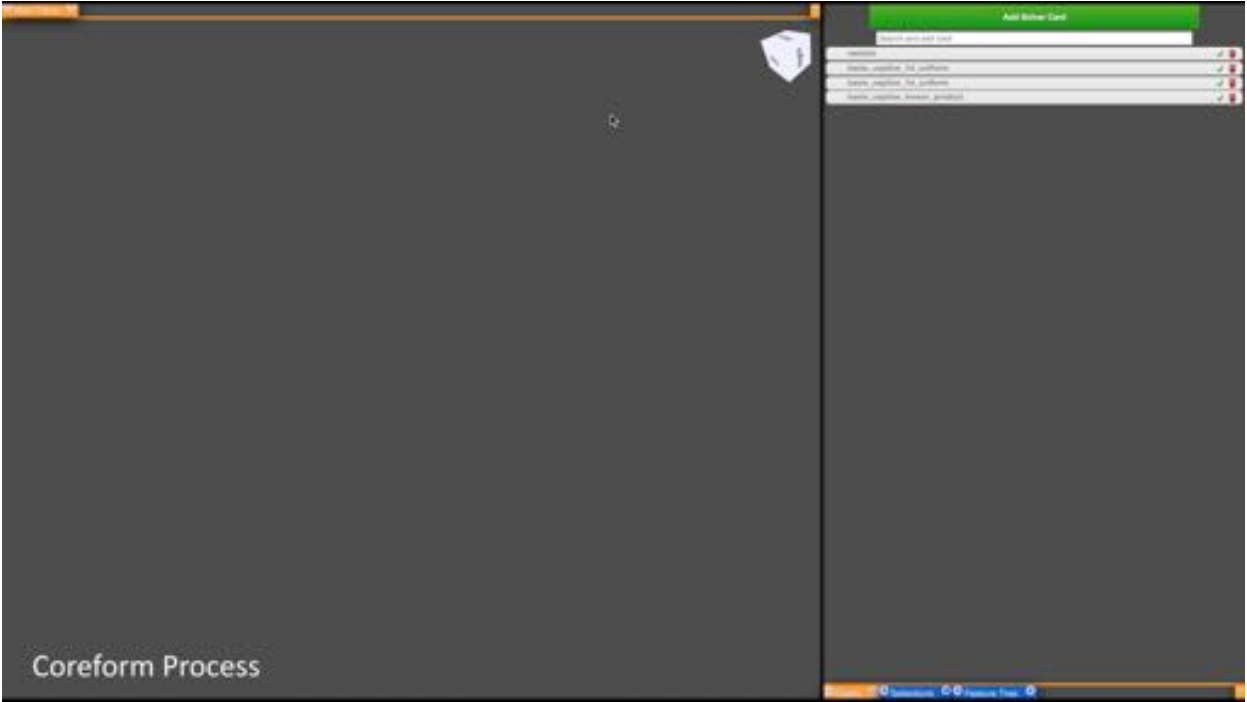
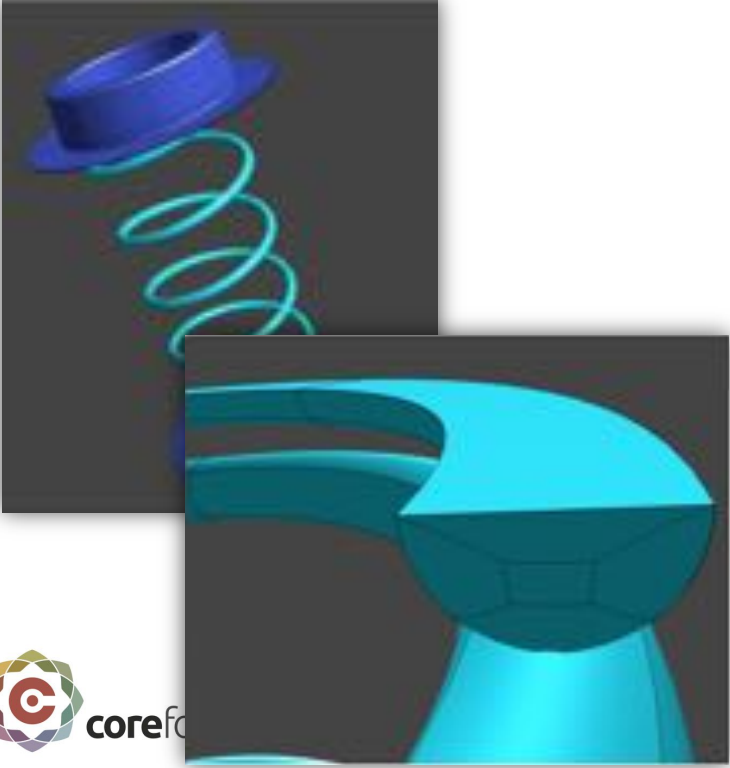
Superior explicit dynamics

Basis Type	Time Step (LS-DYNA)
Linear	1.35×10^{-7}
Multipatch NURBS	1.25×10^{-7} ← Smaller than linear FEA
U-Spline	2.18×10^{-7}

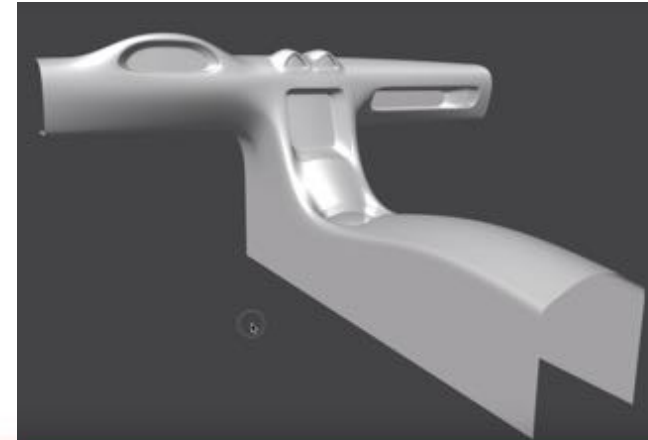
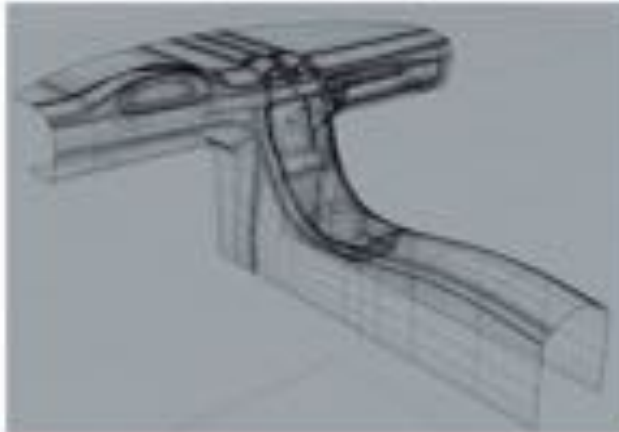
60% larger time step than linear!

2. Import solid spline models

U-spline solid spring model



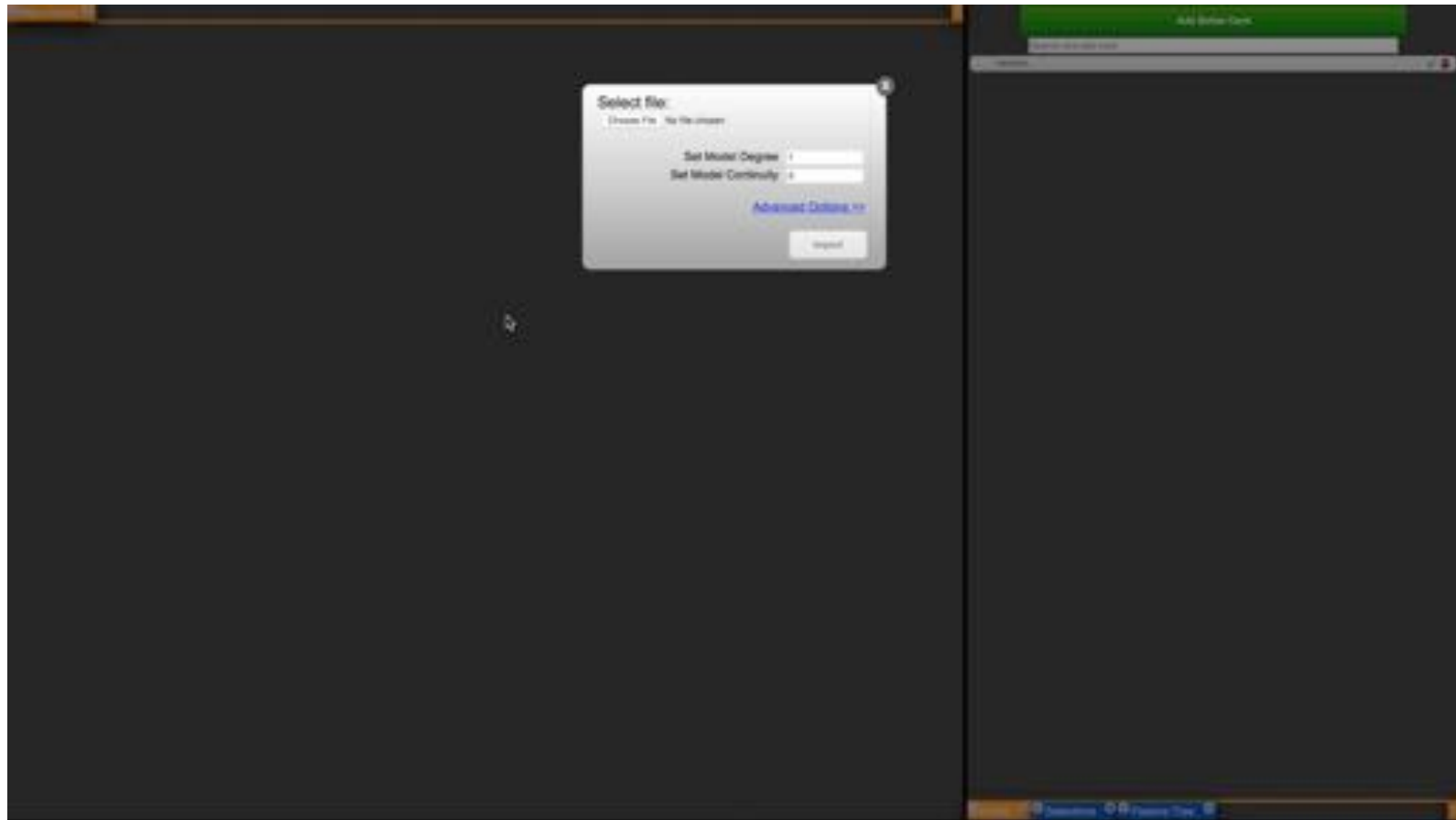
3. Import T-spline CAD model



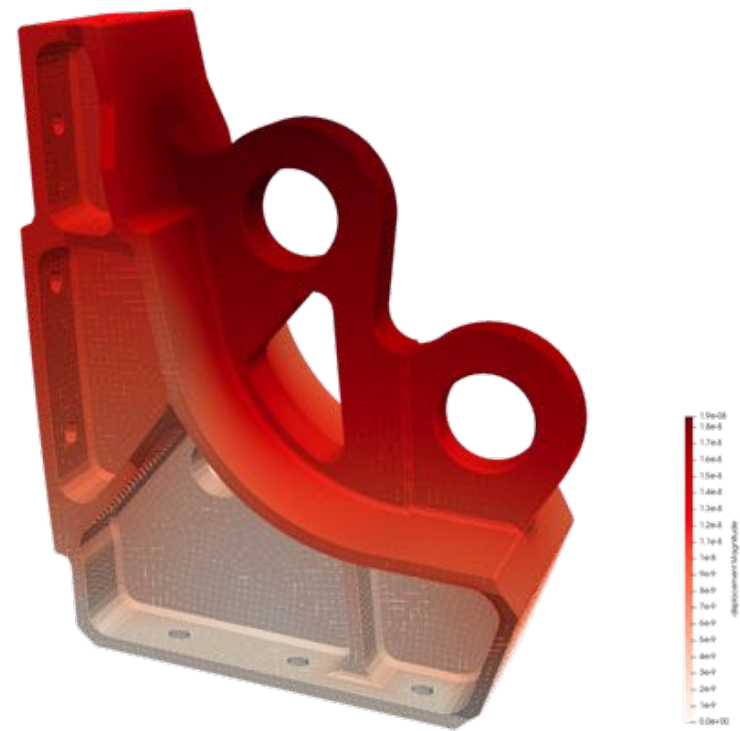
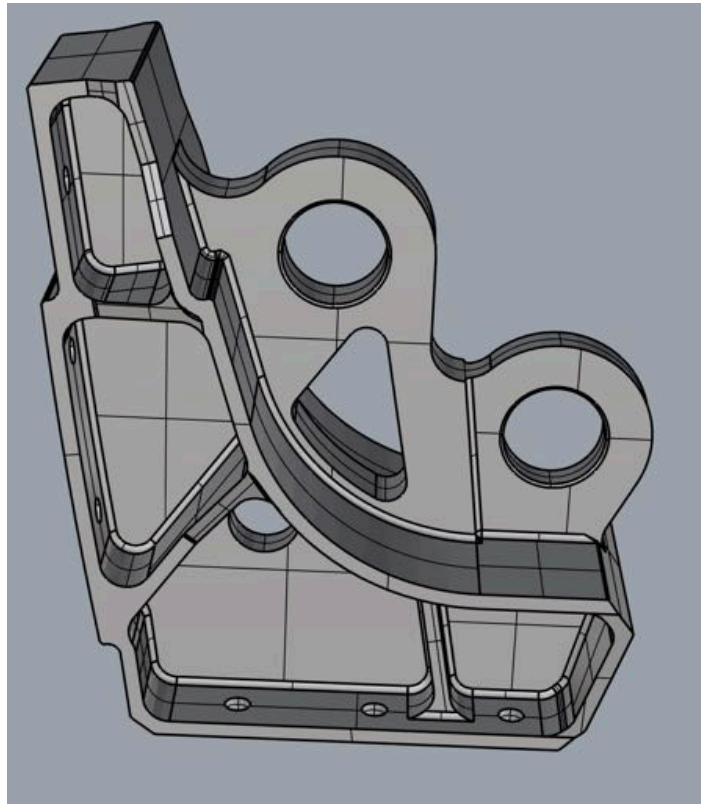
3. Import T-spline CAD model



4. Smooth unstructured FEA mesh via U-splines



4. Smooth unstructured FEA mesh via U-splines

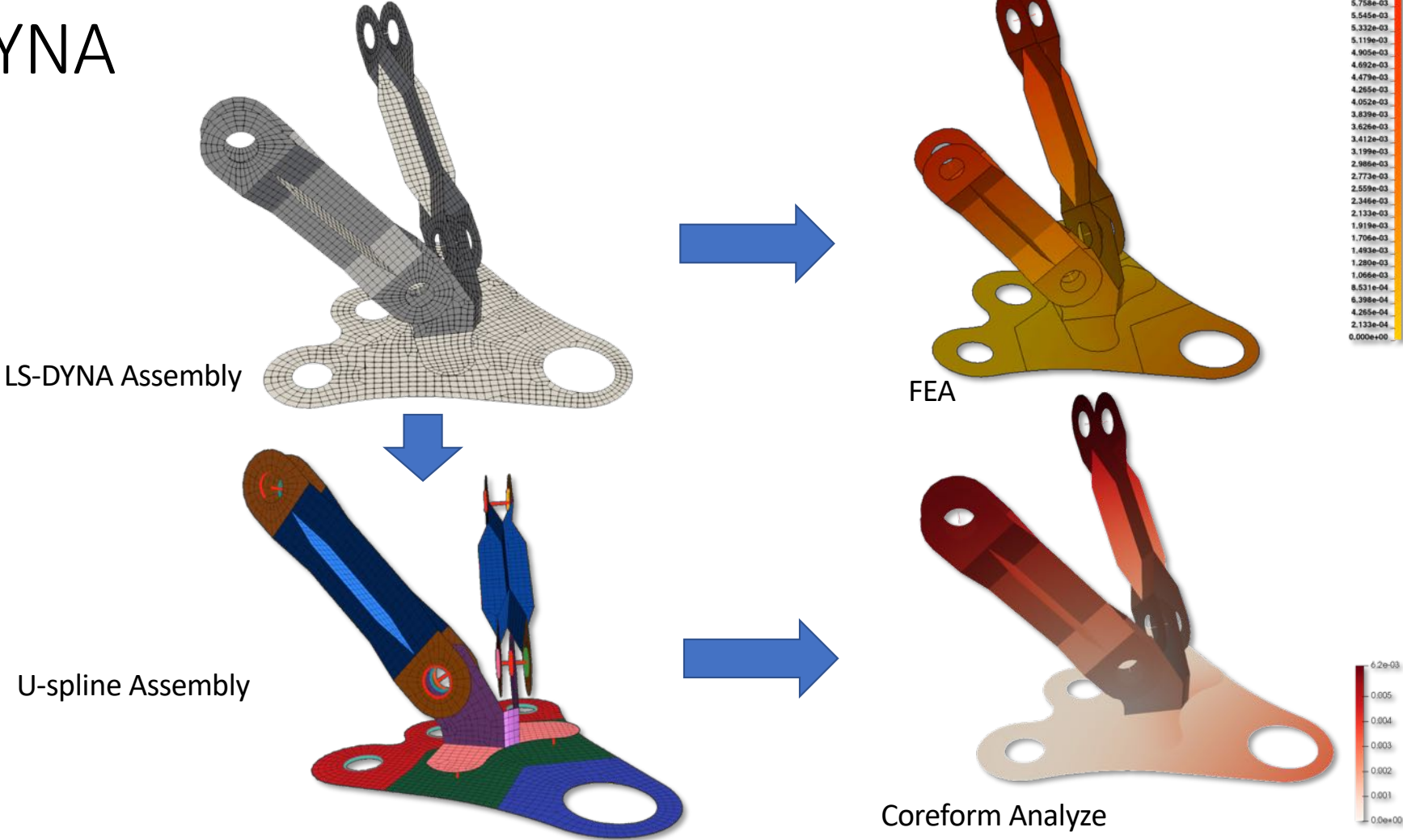


coreform Automatic conversion of solid BREP to U-spline surface. Retopology by Trellis.

4. Smooth unstructured FEA mesh via U-splines

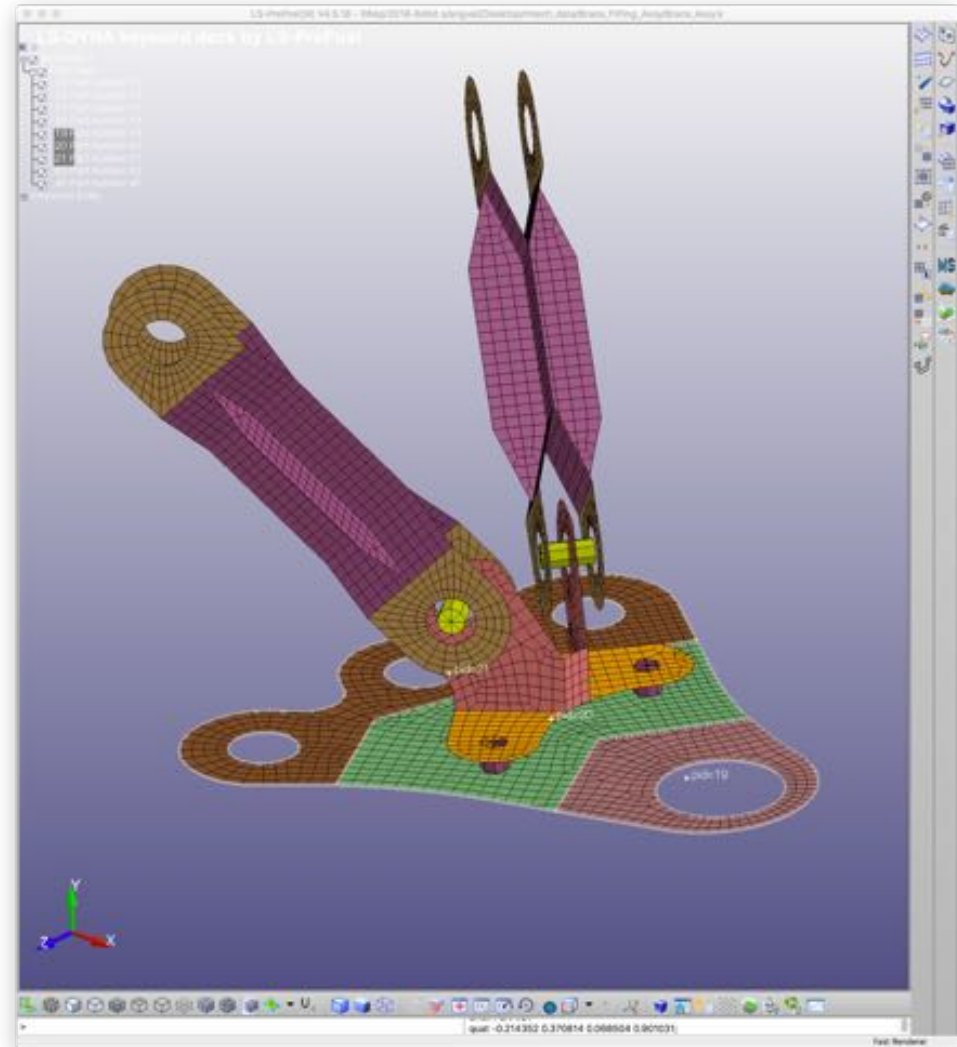


5. Future possibilities: IGA assembly models in LS-DYNA



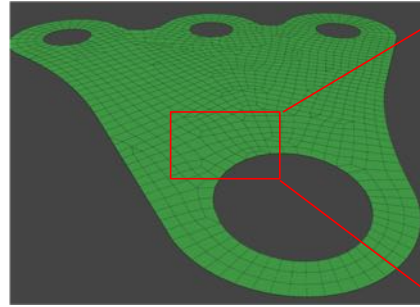
IGA workflow

1. **Import** LS-DYNA assembly
2. **Convert** linear mesh to Degree 2 U-spline, **smooth** element boundaries to be C1 where possible
3. Automatically **translate** material properties, element types, connections
4. **Redefine** applied loads for IGA-suitability
5. **Run** simulation



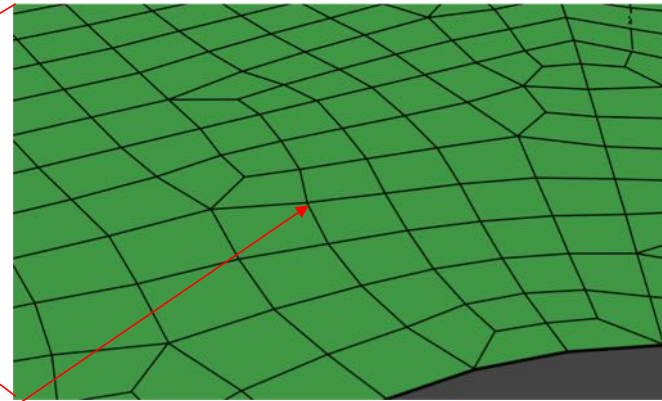
IGA workflow

1. **Import** LS-DYNA assembly
2. **Convert** linear mesh to Degree 2 U-spline, **smooth** element boundaries to be C1 where possible
3. Automatically **translate** material properties, element types, connections
4. **Redefine** applied loads for IGA-suitability
5. **Run** simulation



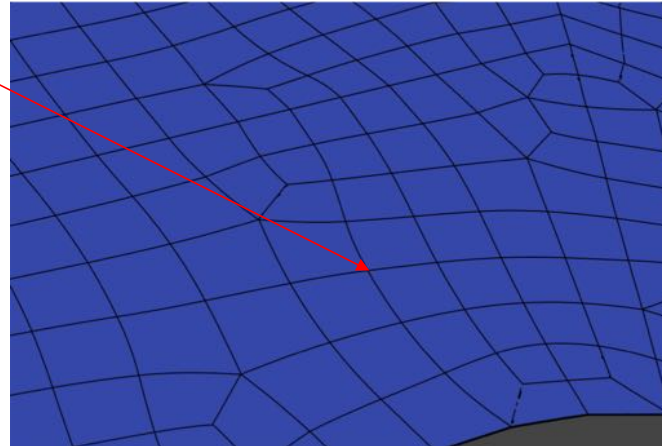
Elements are C0 everywhere.

P1, C0 everywhere:



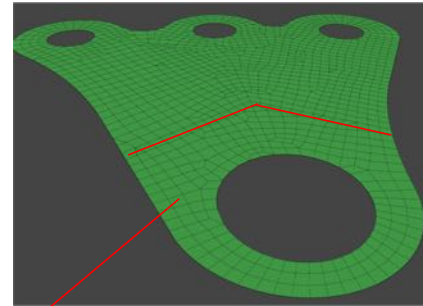
P2, C1 where possible:

Increased smoothness in quadratic mesh

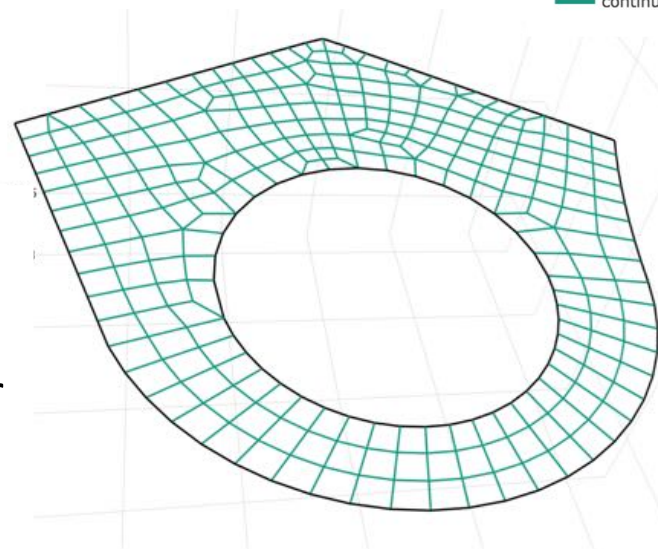


IGA workflow

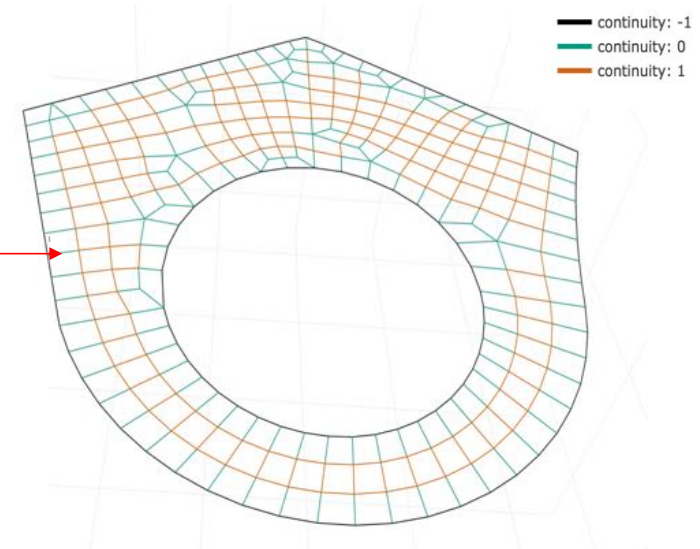
1. **Import** LS-DYNA assembly
2. **Convert** linear mesh to Degree 2 U-spline, **smooth** element boundaries to be C1 where possible
3. Automatically **translate** material properties, element types, connections
4. **Redefine** applied loads for IGA-suitability
5. **Run** simulation



— continuity: -1
— continuity: 0



Section of the original linear mesh

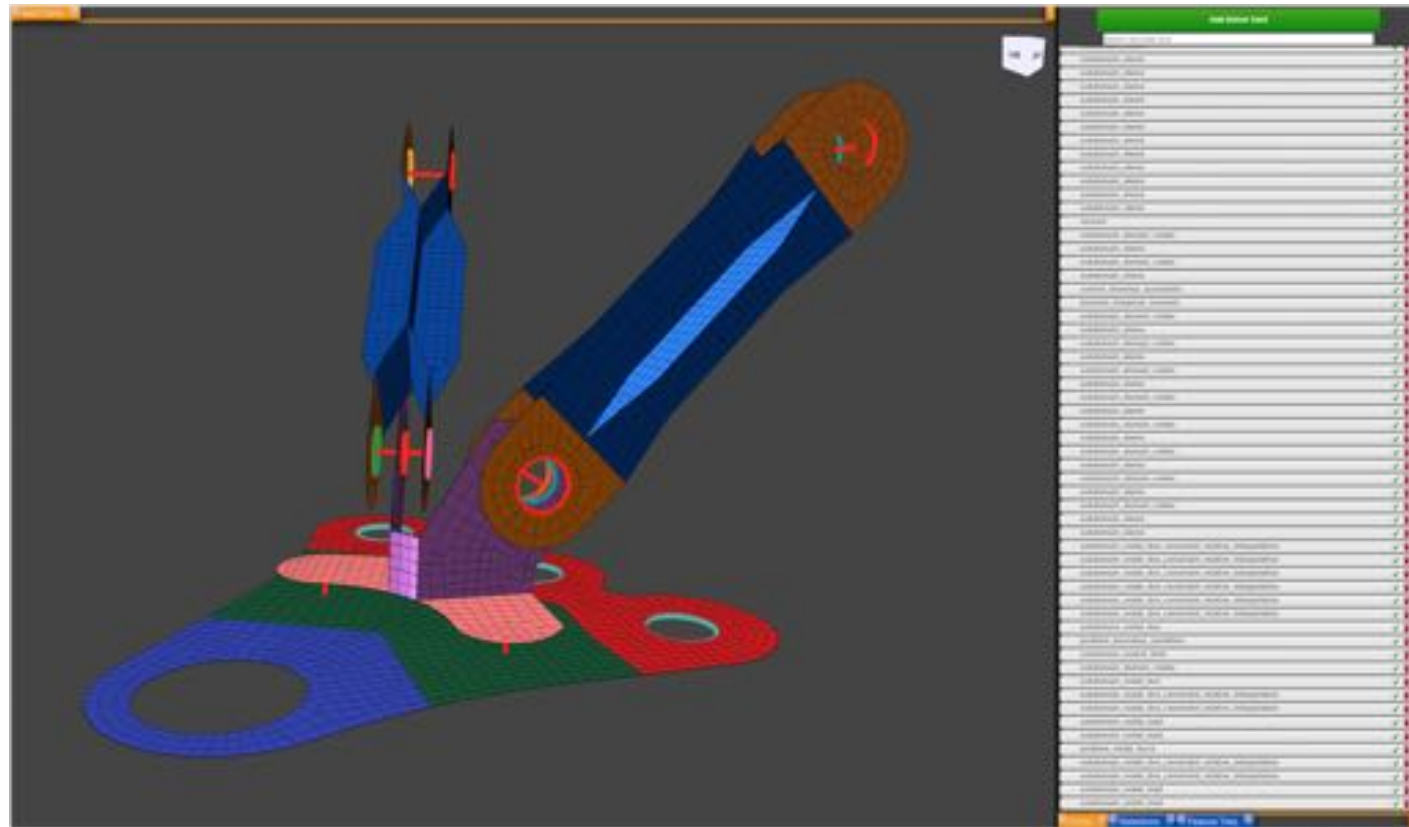


Section of the smoothed U-spline model

Another view of the smoothness (continuity) of the U-spline model

IGA workflow

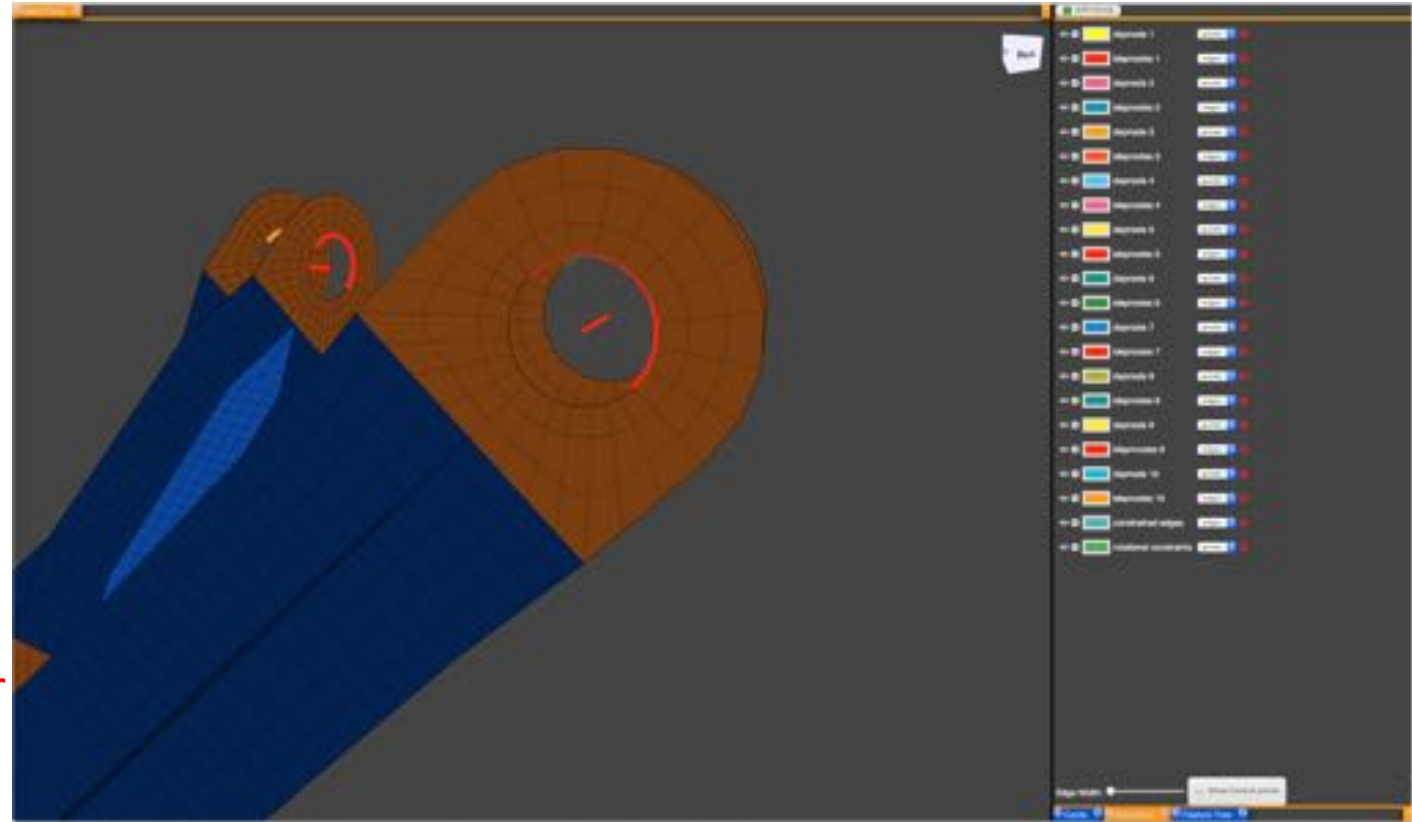
1. **Import** LS-DYNA assembly
2. **Convert** linear mesh to Degree 2 U-spline, **smooth** element boundaries to be C1 where possible
3. **Automatically translate** material properties, element types, connections
4. **Redefine** applied loads for IGA-suitability
5. **Run** simulation



List of cards in the Coreform IGA assembly 

IGA workflow

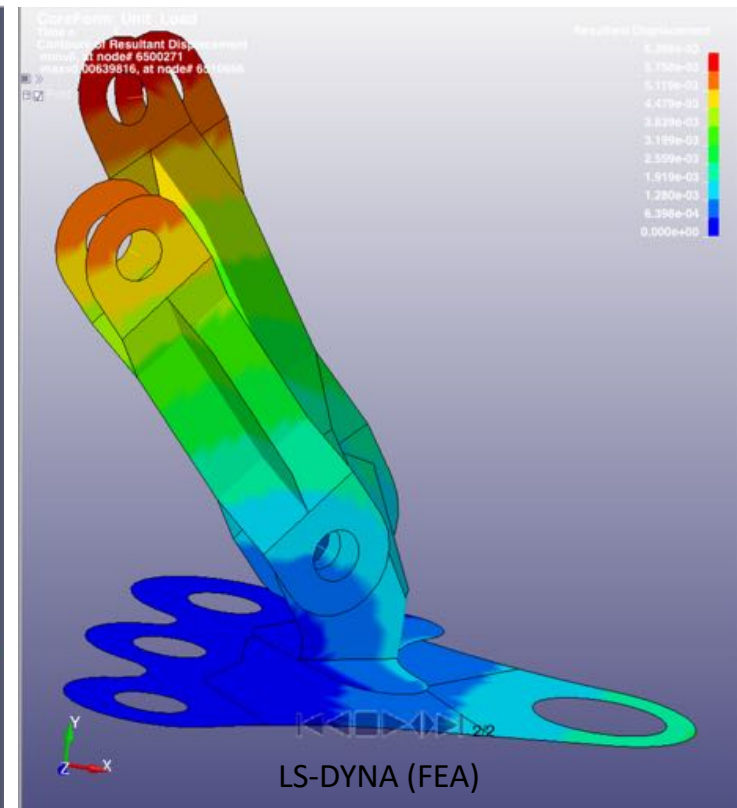
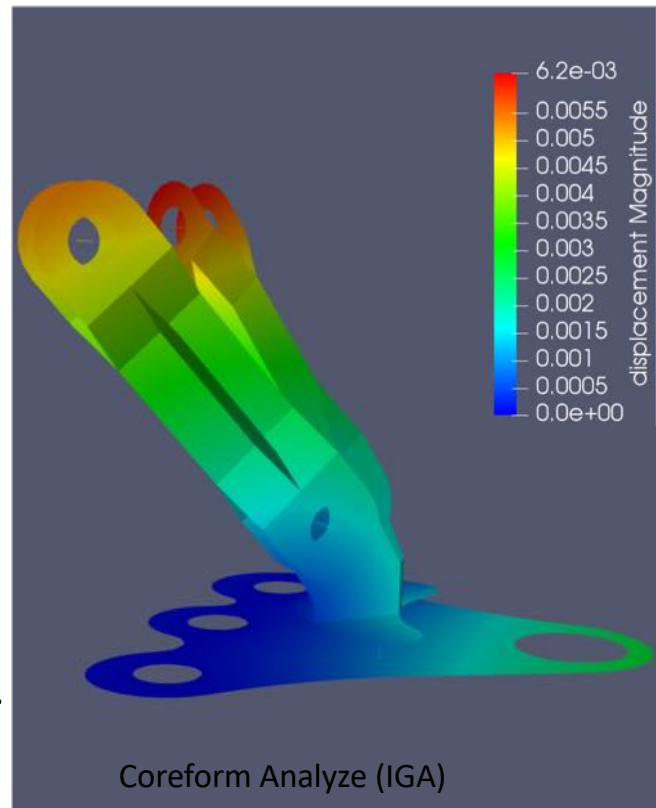
1. **Import** LS-DYNA assembly
2. **Convert** linear mesh to Degree 2 U-spline, **smooth** element boundaries to be C1 where possible
3. Automatically **translate** material properties, element types, connections
4. **Redefine** applied loads for IGA-suitability
5. **Run** simulation



Loads and boundary conditions were assigned directly to the geometry instead of to nodes for improved accuracy.

IGA workflow

1. **Import** LS-DYNA assembly
2. **Convert** linear mesh to Degree 2 U-spline, **smooth** element boundaries to be C1 where possible
3. Automatically **translate** material properties, element types, connections
4. **Redefine** applied loads for IGA-suitability
5. **Run simulation**



We ran the simulation using both Coreform Analyze (IGA) and LS-DYNA (FEA). While the codes use different bases and formulations, the max displacements were within 3% of each other, a strong validation that the underlying physics are correct.

Want to learn more?

IGA short course

- Theory and application
- Coreform offices in Utah, USA
- August 21-22, 2019

IGA 2019

- Annual IGA conference
- Munich, Germany
- September 18-20, 2019

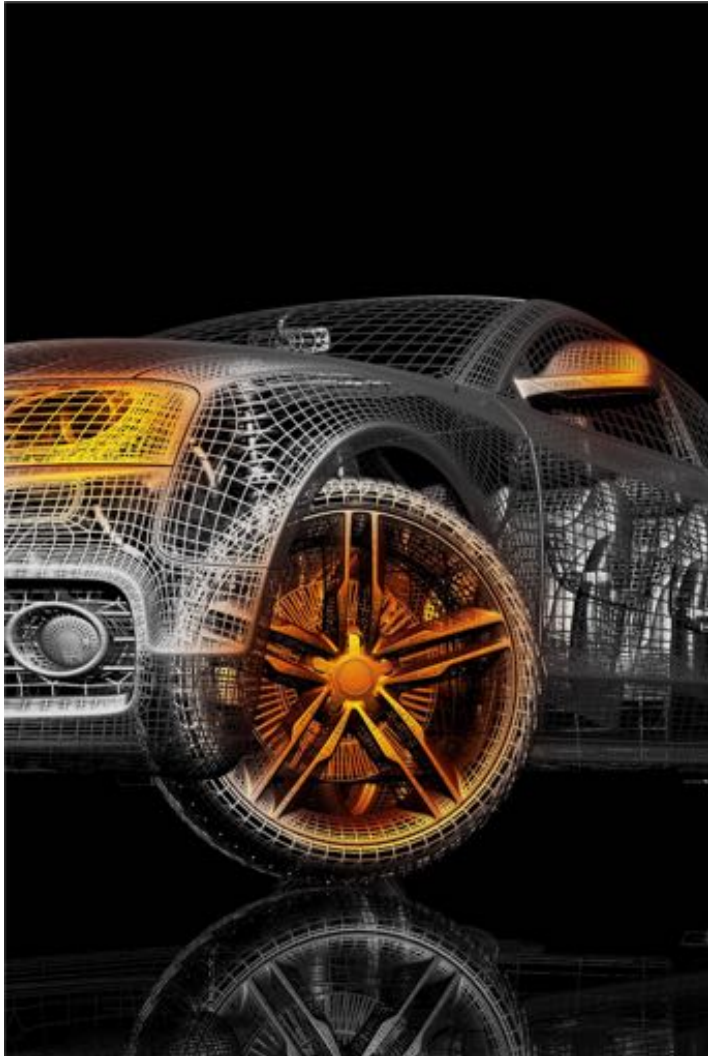
Want to use our beta software?

Come talk with me.

Love IGA?

Come be team member #17 at Coreform.





coreform

Thank you!

Matthew Sederberg, matt@coreform.com